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Love Waves Through Surface Layer in the Presence of a Finite Horizontal Rigid Barrier

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ABSTRACT

The propagation of Love waves in presence of a horizontal rigid barrier of finite length in the surface layer has been discussed. The transmitted waves have been obtained by using Wiener-Hopf technique and Fourier transform. The numerical computation has been done by assuming depth of barrier small as compared to the wavelength of the incident wave. It has been observed that the transmitted waves decrease as the distance from the barrier increases and die out after a very long time. The result of semi-infinite barrier has been obtained as a special case of this problem.

Key words: Rigid barrier, transmitted waves, surface layer, Wiener-Hopf technique

INTRODUCTION

The problems concerning the propagation of seismic waves through crustal layer of earth have been of considerable importance for seismologists since a long time. Such type of study helps the scientists in understanding the internal structure of earth, which in turn can be used for exploration of valuable materials like oil, hydrocarbons, minerals etc. The problems of propagation of Love waves in different media have been discussed by Deshwal and Mudgal (1998), Kar *et al.* (1986), Niazy and Kazi (1980), Wong *et al.* (1995) and Singh (1998). Jardaneh (2004) has considered the expected source of earthquake evaluating the ground source response spectra taking into account local soil properties to evaluate seismic forces. Kaur *et al.* (2005) have studied the reflection and refraction of SH-waves at a corrugated interface between two laterally and vertically heterogeneous viscoelastic solid half-space. Dhaimat and Dhaisat (2006) have studied the sharp cut decrease of Dead Sea. The propagation of wave in inhomogeneous thin film has been discussed by Ugwu *et al.* (2007) using the series expansion solution method of Green's function. Tomar and Kaur (2007) have studied the problem of reflection and transmission of a plane SH-wave at a corrugated interface between a dry sandy half space and an anisotropic elastic half space. They used the Rayleigh method of approximation for studying the effect of sandiness, the anisotropy, the frequency and the angle of incidence on the reflection and transmission coefficients. Ademeso (2009) has discussed the deformation traits in Charnockitic rocks by analyzing the direction of maximum compressional and tensional stresses inferred from the rose diagram. Chattopadhyay *et al.* (2009) has studied the reflection of shear waves in viscoelastic medium at parabolic irregularity. The authors found that the amplitude of reflected wave decreases with increasing length of notch and increases with increasing depth of irregularity. The finite element method analysis has been used by Adedeji and Ige (2011) to investigate and compare the

performance of a reinforce concrete bare frame infilled with or without straw bale wall shape memory alloy diagonal wires subjected to seismic loads and earthquake ground excitation. Ramli and Dawood (2011) have studied the effect of steel fibers on the engineering performance of concrete. A computational technique has been applied to study the field propagation through an inhomogeneous thin film using Lippmann-Schwinger equation by Ugwu (2011). The propagation of seismic waves has also been studied by Zaman (2001), Hai-Ming and Xiao-Fei (2003), Bahdeh *et al.* (2009) and Aziz *et al.* (2011). The problem of Love wave excitation due to interaction between ocean wave and sea bottom topography has been studied by Saito (2010). Here, we discuss the propagation of Love waves through irregularity in form of an infinite rigid strip present in the surface layer.

This study is based on a paper by Sato (1961) who studied the problem of reflection and transmission of Love waves in case the surface layer is variable in thickness. Here we discuss the propagation of Love waves through irregularity in form of a finite rigid horizontal barrier present in the surface layer at finite depth.

THE PROBLEM AND ITS SOLUTION

The propagation of Love waves due to a finite rigid horizontal barrier in the surface layer has been discussed in the present paper. The problem is being analyzed in zx -plane. The z -axis has been taken vertically downwards and x -axis along the interface. The Love wave is normally incident from right to left on a perfectly rigid screen $-l < x < 0$; $z = -h$. The geometry of the problem is shown in Fig. 1. The incident Love wave is given by:

$$v_{0,1} = A \cos \theta_{2N} H e^{-(\theta_{1N} z + i k_{1N} x)}, z \geq 0, \quad (1)$$

$$v_{0,2} = A \cos \theta_{2N} (z + H) e^{-i k_{1N} x}, -H \leq z \leq 0 \quad (2)$$

Where:

$$\theta_{2N} = \sqrt{k_2^2 - k_{1N}^2}, \theta_{1N} = \sqrt{k_{1N}^2 - k_1^2}, |k_1| < |k_2|, \quad k_1 = \frac{\omega}{\theta_1}, \quad k_{1N} = \frac{\omega}{C_{1N}}, \quad (3)$$

and C_{1N} is the phase velocity of n th mode and k_{1N} is the root of equation:

$$\tan \theta_{2N} H = \gamma \frac{\theta_{1N}}{\theta_{2N}}, \gamma = \frac{\mu_1}{\mu_2}, \quad (4)$$

μ_1 and μ_2 being the rigidities of shear waves in the half space and in the crustal layer, respectively.

The wave equation in two dimensions is given as:

$$\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial z^2} + k^2 v = 0 \quad (5)$$

The wave equation in the present study for the surface layer can be written as:

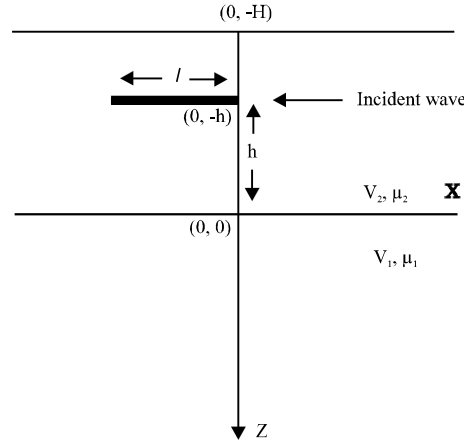


Fig. 1: Geometry of the problem

$$(\nabla^2 + k_j^2)v_j = 0, j=1,2,3 \quad (6)$$

Where:

$$k_j = \sqrt{\frac{\omega^2 + i\epsilon\omega}{V_j^2}} = k_j' + ik_j'' \quad (7)$$

V_1 and V_2 are the velocities of shear waves in the half space $z \geq 0$ and in the layer $-H \leq z \leq 0$, respectively.

Let the total displacement be given by:

$$v = v_{0,1} + v_1, z \geq 0, \quad -\infty < x < \infty \quad (8)$$

$$= v_{0,2} + v_2, -h \leq z \leq 0, \quad -\infty < x < \infty \quad (9)$$

$$= v_{0,2} + v_3, -H \leq z \leq -h, \quad -\infty < x < \infty \quad (10)$$

The boundary conditions are:

$$v_{0,2} + v_2 = 0, \quad z = -h+0, \quad -l \leq x \leq 0 \quad (11)$$

$$v_{0,2} + v_3 = 0, \quad z = -h-0, \quad -l \leq x \leq 0, \quad (12)$$

$$\frac{\partial v_3}{\partial z} = 0, \quad z = -H, \quad -\infty < x < \infty \quad (13)$$

$$v_2 = v_3, \quad \frac{\partial v_2}{\partial z} = \frac{\partial v_3}{\partial z}, \quad z = -h, \quad -\infty < x < -l, \quad 0 < x < \infty \quad (14)$$

$$v_1 = v_2, \quad \mu_1 \frac{\partial v_1}{\partial z} = \mu_2 \frac{\partial v_2}{\partial z}, \quad z = 0, \quad -\infty < x < \infty \quad (15)$$

The boundary conditions (11) and (12) specify that the barrier is rigid and no displacement takes place across the barrier. Using boundary conditions (11) and (12), we have:

$$v_2 = -A \cos \theta_{2N} (z + H) e^{-ik_1 x}, \quad z = -h + 0, \quad -1 \leq x \leq 0 \quad (16)$$

$$v_3 = -A \cos \theta_{2N} (z + H) e^{-ik_1 x}, \quad z = -h - 0, \quad -1 \leq x \leq 0 \quad (17)$$

Taking Fourier transform of Eq. 6, we obtain:

$$\frac{d^2 \bar{v}_j(p, z)}{dz^2} - \theta_j^2 \bar{v}_j(p, z) = 0 \quad (18)$$

where, $\theta_j = \pm \sqrt{p^2 - k_j^2}$ represents Fourier transform of $v_j(x, z)$ which can be defined as:

$$\begin{aligned} \bar{v}_j(p, z) &= \int_{-\infty}^{\infty} v_j(x, z) e^{ipx} dx, \quad p = \alpha + i\beta, \\ &= \int_{-\infty}^{-1} v_j(x, z) e^{ipx} dx + \int_{-1}^0 v_j(x, z) e^{ipx} dx + \int_0^{\infty} v_j(x, z) e^{ipx} dx \\ &= \bar{v}_{j-}(p, z) + \bar{v}_j(p, z) + \bar{v}_{j+}(p, z) \end{aligned} \quad (19)$$

If for a given z , as $|x| \rightarrow \infty$ and $M, \tau > 0$, $|v_j(x, z)| \sim Me^{-\tau|x|}$, then $\bar{v}_{j+}(p, z)$ is analytic in $\beta > -\tau$ and $\bar{v}_{j-}(p, z)$ is analytic in $\beta < \tau$ ($= \text{Im}(k)$). So by analytic continuation $\bar{v}_j(p, z)$ and its derivatives are analytic in the strip $-\tau < \beta < \tau$ in the complex p -plane. Solving Eq. 18 and choosing the sign of θ_j such that its real part is always positive, we obtain:

$$\bar{v}_1(p, z) = A(p) e^{-\theta_1 z}, \quad z \geq 0, \quad (20)$$

$$\bar{v}_2(p, z) = B(p) e^{-\theta_2 z} + C(p) e^{\theta_2 z}, \quad -H \leq z \leq 0 \quad (21)$$

Solving Eq. 21 by using boundary condition (15), we get:

$$\bar{v}_{2-}(p, z) + \bar{v}_2(p, z) + \bar{v}_{2+}(p, z) = A(p) \frac{[\theta_2 \cosh \theta_2 z - \gamma \theta_1 \sinh \theta_2 z]}{\theta_2} \quad (22)$$

Differentiating above equation with respect to z and putting $z = -h$ and denoting $\bar{v}_j(p, -h)$ by $\bar{v}_j'(p)$ etc. and then eliminating $A(p)$, we obtain:

$$\bar{v}_{2+}(p, z) + \bar{v}_2(p, z) + \bar{v}_{2-}(p, z) = -\frac{\theta_2 \cosh \theta_2 z - \gamma \theta_1 \sinh \theta_2 z}{\theta_2 (\theta_2 \sinh \theta_2 h + \gamma \theta_1 \cosh \theta_2 h)} \times [\bar{v}_{2+}'(p) + \bar{v}_2'(p) + \bar{v}_{2-}'(-p)] \quad (23)$$

Solving Eq. 18 for $j = 3$, using boundary condition (13), we have

$$\bar{v}_{3+}(p, z) + \bar{v}_3(p, z) + \bar{v}_{3-}(p, z) = 2D(p) \cosh \theta_2 (z + H) e^{\theta_2 H} \quad (24)$$

Differentiating above equation with respect to z and putting z = -h and denoting $\bar{v}_j'(p, -h)$ by $\bar{v}_j'(p)$ etc. and then eliminating D (p) we obtain:

$$\bar{v}_{3+}(p, z) + \bar{v}_3(p, z) + \bar{v}_{3-}(p, z) = \frac{1}{\theta_2} \cdot \frac{\cosh \theta_2(z+H)}{\sinh \theta_2 \delta} \times [\bar{v}_{3+}'(p) + \bar{v}_3'(p) + \bar{v}_{3-}'(p)] \quad (25)$$

where, $\delta = H-h$.

Taking Fourier transformation of Eq. 14:

$$\bar{v}_{2+}(p) = \bar{v}_{3+}(p); \quad \bar{v}_{2+}'(p) = \bar{v}_{3+}'(p) \text{ and } \bar{v}_{2-}(p) = \bar{v}_{3-}(p); \quad \bar{v}_{2-}'(p) = \bar{v}_{3-}'(p) \quad (26)$$

From Eq. 16 and 17, we can write in usual notation as:

$$\bar{v}_2(p) = \bar{v}_3(p) = \frac{iA \cos(\theta_{2N} \delta) e^{ik_N x}}{p - k_{1N}} \times \{1 - e^{-i(p-k_N)x}\} \quad (27)$$

Now using Eq. 26 and 27 in Eq. 25 for z = -h we have:

$$\bar{v}_{2+}(p) + \bar{v}_2(p) + \bar{v}_{2-}(p) = \frac{\coth \theta_2 \delta}{\theta_2} \times \{\bar{v}_{2+}'(p) + \bar{v}_3'(p) + \bar{v}_{2-}'(p) + \bar{v}_2'(p) - \bar{v}_2(p)\} \quad (28)$$

Now from Eq. 23 and 28 for z = -h, we can write:

$$[\bar{v}_{2+}(p) + \bar{v}_2(p) + \bar{v}_{2-}(p)] \frac{\theta_2}{\cosh \theta_2 \delta} \frac{f_1(p)}{f_2(p)} = -[\bar{v}_{2+}'(p) + \bar{v}_3'(p) + \bar{v}_{2-}'(p) + \bar{v}_2'(p) - \bar{v}_2(p)] \quad (29)$$

Where:

$$f_1(p) = \theta_2 \sinh \theta_2 H + \gamma \theta_1 \cosh \theta_2 H \quad (30)$$

$$f_2(p) = \theta_2 \cosh \theta_2 H + \gamma \theta_1 \sinh \theta_2 h \quad (31)$$

The Eq. 29 is the Wiener-Hopf type differential equation discussed by Noble (1958).

SOLUTION OF WIENER-HOPF EQUATION

Now using Eq. 27 and 29 may be written as:

$$\bar{v}_{2+}(p) + \bar{v}_{2-}(p) - \{\bar{v}_3'(p) - \bar{v}_2'(p)\} \frac{\cosh \theta_2 \delta}{\theta_2} \frac{f_2(p)}{f_1(p)} = \frac{B \{1 - e^{-i(p-k_N)x}\}}{p - k_{1N}} \quad (32)$$

Where:

$$B = -iA \cos \theta_{2N} \delta e^{ik_N x} \quad (33)$$

Now we factorize $\left(\frac{1}{\cosh\theta_2\delta}\right)\frac{f_1(p)}{f_2(p)}$ as discussed by Sato (1961) as:

$$\left(\frac{1}{\cosh\theta_2\delta}\right)\frac{f_1(p)}{f_2(p)} = K_+(p)K_-(p) \quad (34)$$

Let $p = \pm k_{1m}$ and $p = \pm k_{2m}$ are the zeros of $f_1(p)$ and $f_2(p)$, respectively. Then we write:

$$\frac{f_1(p)}{f_2(p)} = \prod_{m=1}^{\infty} \frac{(p^2 - k_{1m}^2) G_1(p)}{(p^2 - k_{2m}^2) G_2(p)} \quad (35)$$

Where:

$$G_1(p) = \frac{f_1(p)}{\prod_{m=1}^{\infty} (p^2 - k_{1m}^2)} \text{ and } G_2(p) = \frac{f_2(p)}{\prod_{m=1}^{\infty} (p^2 - k_{2m}^2)} \quad (36)$$

and $G_1(p)$ and $G_2(p)$ have no zeros. Also we can write:

$$L(p) = \frac{G_1(p)}{G_2(p)} = L_+(p)L_-(p) \quad (37)$$

Where:

$$\log L_+(p) = \frac{1}{\pi} \int_0^{\infty} \frac{\phi_1 - \phi_2}{t - ip} dt - \frac{1}{\pi} \int_0^{h_1} \frac{\phi_1 - \phi_2}{t + p} dt \quad (38)$$

Where:

$$\tan \phi_1 = \frac{\gamma(t^2 + k_1^2)^{1/2} \cos H(t^2 + k_2^2)^{1/2}}{(t^2 + k_2^2)^{1/2} \sin H(t^2 + k_2^2)^{1/2}} \quad (39)$$

$$\tan \phi_2 = \frac{\gamma(k_1^2 - t^2)^{1/2} \cos H(k_2^2 - t^2)^{1/2}}{(k_2^2 - t^2)^{1/2} \sin H(k_2^2 - t^2)^{1/2}} \quad (40)$$

$\tan \phi_2$ and $\tan \phi_1$ are obtained from Eq. 39 and 40 by replacing H by h. Now, we write:

$$\frac{1}{\cosh\theta_2\delta} \frac{f_1(p)}{f_2(p)} = \frac{L_+(p)L_-(p)}{H_+(p)H_-(p)} \prod_{m=1}^{\infty} \frac{(p^2 - k_{1m}^2)}{(p^2 - k_{2m}^2)} = K_+(p)K_-(p) \quad (41)$$

Where:

$$K_+(p) = K_-(p) = \frac{L_+(p)}{H_+(p)} \prod_{m=1}^{\infty} \frac{(p + k_{1m})}{(p + k_{2m})} \quad (42)$$

and $|K_+(p)| \rightarrow |p|^{1/2}$, as $|p| \rightarrow \infty$.

Now $\theta_2 = \sqrt{p^2 - k_2^2}$ can be factorized as:

$$\theta_2 = \sqrt{p^2 - k_2^2} = e^{-\frac{i\pi}{4}} \sqrt{p+k_2} \times e^{\frac{i\pi}{4}} \sqrt{p-k_2} \quad (43)$$

Using Eq. 34 and 43, Eq. 32 can be written as:

$$\bar{v}_{2+}(p) + \bar{v}_{2-}(p) - \frac{\{\bar{v}_3(p) - \bar{v}_2(p)\}}{Q_+(p)Q_-(p)} = \frac{B\{1 - e^{-i\pi(p-k_{IN})}\}}{p - k_{IN}} \quad (44)$$

Where:

$$Q_{\pm}(p) = e^{\pm \frac{i\pi}{4}} \sqrt{p \pm k_2} K_{\pm}(p) \text{ and } Q_+(-p) = Q_-(p) \quad (45)$$

Similarly, Eq. 34 may also be written as:

$$\begin{aligned} \bar{v}_{2+}(p)Q_+(p) + \frac{B\{Q_+(p) - Q_+(k_{IN})\}}{p - k_{IN}} + N_+(p) + M_+(p) &= \frac{\{\bar{v}_3(p) - \bar{v}_2(p)\}}{Q_-(p)} \\ -N_-(p) - M_-(p) - \frac{BQ_+(k_{IN})}{p - k_{IN}} & \end{aligned} \quad (46)$$

Where:

$$N_+(p) + N_-(p) = e^{i\pi} \bar{v}_{2-}(p) Q_+(p) \quad (47)$$

and:

$$M_+(p) + M_-(p) = \frac{B e^{-i\pi(p-k_{IN})}}{p - k_{IN}} Q_+(p) \quad (48)$$

Also, multiplying Eq. 32 by $e^{i\pi}$ and rearranging the terms, we have:

$$\bar{v}_{2-}(p)Q_-(p) + \frac{BQ_-(p)e^{i\pi k_{IN}}}{p - k_{IN}} + R_-(p) - T_-(p) = T_+(p) - R_+(p) + \frac{e^{-i\pi}}{Q_+(p)} \times \{\bar{v}_3(p) - \bar{v}_2(p)\} \quad (49)$$

Where:

$$R_+(p) + R_-(p) = e^{i\pi} \bar{v}_{2+}(p) Q_-(p) \quad (50)$$

and:

$$T_+(p) + T_-(p) = \frac{B e^{i\pi}}{p - k_{IN}} Q_-(p) \quad (51)$$

Also, we make following substitutions for simplicity:

$$P_{1,2} = \frac{Q_+(\mathbf{p}) - Q_+(\pm \mathbf{k}_{1N})}{\mathbf{p} \mp \mathbf{k}_{1N}}, \quad Q_1(\mathbf{p}) = P_1(\mathbf{p}) - e^{i\mathbf{k}_{1N}} R_1(\mathbf{p}), \quad Q_2(\mathbf{p}) = e^{i\mathbf{k}_{1N}} P_2(\mathbf{p}) - R_2(\mathbf{p}) \quad (52)$$

Where:

$$R_1(\mathbf{p}) = \frac{1}{2\pi i} \int_{-\infty+i\beta}^{\infty+i\beta} \frac{Q_-(\alpha) e^{i\alpha \cdot 1}}{(\alpha + \mathbf{p})(\alpha + \mathbf{k}_{1N})} d\alpha \quad (53)$$

and:

$$R_2(\mathbf{p}) = \frac{1}{2\pi i} \int_{-\infty+i\beta}^{\infty+i\beta} \frac{Q_-(\alpha) e^{i\alpha \cdot 1}}{(\alpha + \mathbf{p})(\alpha - \mathbf{k}_{1N})} d\alpha - \frac{Q_-(\mathbf{k}_{1N}) e^{i\alpha \cdot 1}}{\mathbf{p} + \mathbf{k}_{1N}} \quad (54)$$

Now Eq. 23 and 25 may respectively be written as:

$$\bar{v}_2(\mathbf{p}, z) = \frac{\theta_2 \cosh \theta_2 z - \gamma \theta_1 \sinh \theta_2 z}{\theta_2 \cosh \theta_2 h + \gamma \theta_1 \sinh \theta_2 h} \times \bar{v}_2(\mathbf{p}) \quad (55)$$

and:

$$\bar{v}_3(\mathbf{p}, z) = \frac{\cosh \theta_2 (z + H)}{\cosh \theta_2 \delta} \times \bar{v}_2(\mathbf{p}) \quad (56)$$

Where:

$$\begin{aligned} \bar{v}_2(\mathbf{p}) = & -\frac{B(\mathbf{k}_2 + \mathbf{k}_{1N}) K_+(\mathbf{k}_{1N})}{(\mathbf{p} - \mathbf{k}_{1N}) \sqrt{\mathbf{p} + \mathbf{k}_2 K_+(\mathbf{p})}} - \frac{BR_1(\mathbf{p}) e^{\left\{i(\mathbf{k}_{1N} + \frac{\pi}{4})\right\}}}{\sqrt{\mathbf{p} + \mathbf{k}_2 K_+(\mathbf{p})}} + \frac{BC_1 T(\mathbf{p}) e^{\frac{i\pi}{4}}}{\sqrt{\mathbf{p} + \mathbf{k}_2 K_+(\mathbf{p})}} \\ & + \frac{B e^{i(\mathbf{k}_{1N} - \mathbf{p})} \sqrt{\mathbf{k}_{1N} - \mathbf{k}_2 K_-(\mathbf{k}_{1N})}}{(\mathbf{p} - \mathbf{k}_{1N}) \sqrt{\mathbf{p} - \mathbf{k}_2 K_-(\mathbf{p})}} - \frac{BR_2(-\mathbf{p}) e^{\left\{-i(\mathbf{p} + \frac{\pi}{4})\right\}}}{\sqrt{\mathbf{p} - \mathbf{k}_2 K_-(\mathbf{p})}} + \frac{BC_2 T(-\mathbf{p}) e^{-i(\mathbf{p} + \frac{\pi}{4})}}{\sqrt{\mathbf{p} - \mathbf{k}_2 K_-(\mathbf{p})}} \end{aligned} \quad (57)$$

The displacement $v_2(x, z)$ is obtained by inversion of Fourier transform of Eq. 55 as given below:

$$\begin{aligned} v_2(x, z) = & \frac{1}{2\pi} \int_{-\infty+i\beta}^{\infty+i\beta} \bar{v}_2(\mathbf{p}, z) e^{-i\mathbf{p}x} d\mathbf{p} \\ = & \frac{1}{2\pi} \int_{-\infty+i\beta}^{\infty+i\beta} \frac{\theta_2 \cosh \theta_2 z - \gamma \theta_1 \sinh \theta_2 z}{\theta_2 \cosh \theta_2 h + \gamma \theta_1 \sinh \theta_2 h} \times \bar{v}_2(\mathbf{p}) e^{-i\mathbf{p}x} d\mathbf{p} \end{aligned} \quad (58)$$

Also, the displacement $v_3(x, z)$ is obtained by inversion of Fourier transform of Eq. 56 as given below:

$$v_3(x, z) = \frac{1}{2\pi} \int_{-\infty+i\beta}^{\infty+i\beta} \bar{v}_3(p, z) e^{-ipx} dp \quad (59)$$

$$= \frac{1}{2\pi} \int_{-\infty+i\beta}^{\infty+i\beta} \frac{\cosh \theta_2(z+H)}{\cosh \theta_2 \delta} \times \bar{v}_2(p) e^{-ipx} dp$$

where, $\bar{v}_2(p)$ is given in Eq. 57.

RESULTS AND DISCUSSION

For finding different component of waves, we evaluate the integral in Eq. 58 and Eq. 59 in different regions. For evaluation of Eq. 58, as anticipated, there is a pole at $p = k_{1N}$ having no contribution. Furthermore, let $p = k_{2m}$ be the roots of Eq. $f_2(p) = \theta_2 \cosh \theta_2 h + \gamma \theta_1 \sinh \theta_2 h = 0$. The residue due to this pole contribute to:

$$v_{2,1}(x, z) = -\sum_{m=1}^{\infty} \left[-\frac{B\sqrt{k_2 + k_{1N}} K_+(k_{1N})}{k_{2m} - k_{1N}} - Be^{i(k_{1N} + \frac{\pi}{4})} R_1(k_{2m}) + Be^{i\frac{\pi}{4}} T(k_{2m}) C_1 \right] \left(\frac{C_{2m}}{U_{2m}} - 1 \right) \quad (60)$$

$$\times \frac{i \sin \theta_{2m}(z+h) k_{2m}}{\theta_{2m} h K_+(k_{2m}) \sqrt{k_2 + k_{2m}}} e^{-ik_{2m}x}$$

where, $\theta_{2m} = \sqrt{k_2^2 - k_{2m}^2}$.

Equation 60 represents the transmitted waves in the region $-h \leq z \leq 0$; $-l \leq x \leq 0$. The first term in this equation represents the component of diffracted wave at the edge $x = 0$, while other terms are the interaction terms due to second edge. Similarly, the pole at $p = k_{1m}$ contributes to:

$$v_{2,2}(x, z) = -\sum_{m=1}^{\infty} \left[\frac{B\sqrt{k_{1N} - k_2} K_-(k_{1N})}{k_{1m} - k_{1N}} e^{i(k_{1N} - k_{1m})} - Be^{-i(k_{1m} + \frac{\pi}{4})} R_2(-k_{1m}) + Be^{-i(k_{1m} + \frac{\pi}{4})} T(-k_{1m}) C_2 \right] \quad (61)$$

$$\times \frac{\cos(\theta_{2m} \delta) \cos \theta_{2m}(z+H) k_{2m} K_+(k_{1m}) k_{1m}}{\theta_{2m} H \sqrt{k_{1m} - k_2}} \left(\frac{C_{1m}}{U_{1m}} - 1 \right) e^{-ik_{1m}x}$$

The Eq. 61 represents the transmitted waves in the region $-h \leq z \leq 0$, $-\infty \leq x \leq -l$ and the first term represents the diffracted component of waves at the edge $x = -l$.

Also:

$$C_{2m} = \frac{\omega}{k_{2m}}$$

and:

$$C_{1m} = \frac{\omega}{k_{1m}}$$

are the phase velocities of Love type waves of m th mode in the layered structure with a layer of uniform thickness h .

Now we find the transmitted waves in the region $-H \leq z \leq -h$; $x \leq 0$. There is a pole at $p = k_{1N}$, the contribution due to which is zero. The poles at:

$$p = ip_n = \left\{ k_2^2 - \frac{(2n-1)^2 \pi^2}{4\delta^2} \right\}^{1/2}$$

$n = 1, 2, 3, \dots$, contributes to:

$$v_{3,1}(x, z) = \sum_{n=1}^{\infty} \frac{(-1)^{n+1} i \cos\left(\frac{(2n-1)\pi}{2\delta}(z+H)\right) e^{-i\left\{k_2^2 - \frac{(2n-1)^2 \pi^2}{4\delta^2}\right\}^{1/2} x}}{K_+(ip_n) \sqrt{k_2 + ip_n}} \times \left\{ \frac{-B\sqrt{k_{1N} + k_2} K_+(k_{1N})}{ip_n - k_{1N}} - B e^{i(k_{1N} + \frac{\pi}{4})} R_1(ip_n) + B C_1 T(ip_n) e^{\frac{i\pi}{4}} \right\} \quad (62)$$

Equation 62 represents the transmitted waves in the region $-H \leq z \leq -h$; $-l \leq x \leq 0$. The poles at $p = k_{2m}$ contributes to:

$$v_{3,2}(x, z) = - \sum_{m=1}^{\infty} \left[\frac{B\sqrt{k_{1N} - k_2} K_-(k_{1N})}{k_{1m} - k_{1N}} e^{i(k_{1N} - k_{1m})} - B e^{-i(k_{1m} + \frac{\pi}{4})} R_2(-k_{1m}) + B e^{-i(k_{1m} + \frac{\pi}{4})} T(-k_{1m}) C_2 \right] \times \frac{\cos(\theta_{2m} \delta) \cos \theta_{2m} (z+H) k_{2m} K_+(k_{1m}) k_{1m}}{\theta_{2m} H \sqrt{k_{1m} - k_2}} \left(\frac{C_{1m}}{U_{1m}} - 1 \right) e^{-ik_{1m} x} \quad (63)$$

Equation 63 represents the transmitted waves in the region $-H \leq z \leq -h$; $-\infty \leq x \leq -l$. Clearly, this result is an analytic continuation of the result obtained in Eq. 61.

NUMERICAL COMPUTATION AND ANALYSIS OF RESULTS

The transmitted waves in different regions have been found out in Eq. 60, 61, 62 and 63. For computation purpose we have considered $k_2 \delta$ small as compared to the wavelength of the incident Love waves. We have taken, $V_1 = 4.6 \text{ km sec}^{-1}$, $V_2 = 3.9 \text{ km sec}^{-1}$, $\mu_1 = 7.98 \times 10^{10} \text{ pa}$, $\mu_2 = 4.11 \times 10^{10} \text{ pa}$, $k_2 \delta < 0.01$ for calculation purpose and different waves have been obtained. In the present discussion, we have taken the barrier of finite length. As a limiting case of this problem, if we take $l \rightarrow \infty$, then we have only one edge at $x = 0$ and Eq. 60 will have only the first term, which is same as obtained by Kazi (1975) for a semi-infinite barrier. Also, if we take $l = 0$, i.e., the whole of the surface layer is rigid, the Love wave moves with the velocity of shear waves in the surface layer.

CONCLUSIONS

We studied the problem of propagation of Love waves in the layered media with a surface layer having a horizontal rigid barrier of finite length. The numerical computation shows that the diffracted Love wave decreases as the distance from the barrier increases. It is clear from the discussion that if the barrier of large size is considered, the diffracted wave of larger intensity is observed. So by measuring the component of the wave obtained, the internal structure of earth can be predicted for specific study. The case of semi-infinite barrier is obtained as a special case.

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