Effect of Thickness on Structural, Optical and Sensing Properties of CdS Thin Films Prepared by Ultrasonic Nebulizer Method

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Abstract: Thin films of cadmium sulfide with different thickness (300-600 nm) were deposited on preheated glass substrates (430°C) by Ultrasonic Nebulizer Deposition (UND). The effect of thickness on the structural, optical and gas sensing properties of films has been investigated. X-ray diffraction patterns indicated that the CdS films had a polycrystalline hexagonal structure with preferred orientations along (002) and (101) directions. The crystallite size increases along (002) plane with the thickness increase and attains a maximum 56.68 nm for 600 nm. The surface roughness is decreased with the increase of the films thickness which has been investigated by Atomic Force Microscopy (AFM). It was observed that as the film thickness increases from 300-600 nm the optical band gap blue shifted from 2.35-2.42 eV. The sensing characteristics of the films were studied as a function of operating temperature and for three different concentration (10-30 ppm) of ethanol. The results showed that the sensitivity increases with operating temperature and reached a maximum values 75% at 310°C for the film with 500 nm thicknesses. Moreover, the films showed fast response and recovery times at higher operating temperature.

Key words: CdS, thin films, ultrasonic nebulizer technique, gas sensors, hexagonal structure, AFM

INTRODUCTION

Cadmium sulfide is an 2-4 groups semiconductor it has been used as a suitable window layer, solar cells, photo detectors, lasers and gas sensors (Li *et al.*, 2017; Mathew *et al.*, 2004; Williams *et al.*, 2014). This is because CdS thin films have high transparency, wide and direct bandgap transition (2.42 eV), high electron affinity and n-type conductivity (Mathew *et al.*, 2004; Williams *et al.*, 2014; Chander and Dhaka, 2017). Different methods have been used to prepare CdS thin films which include RF sputtering (Williams *et al.*, 2014), electron beam vacuum evaporation (Chander and Dhaka, 2017), Chemical Bath Deposition (CBD) (Kumar *et al.*, 2009), physical evaporation (Nesheva *et al.*, 2006).

Polycrystalline CdS based gas sensors are commercially important for detecting reducible gases such as hydrogen, methane, butane ethanol and ammonia with high sensitivities. It is well known that the gas adsorption onto the surface of a semiconductor can influence its electrical conductivity. In fact, conductivity of semiconductor gas sensor changes by few orders of magnitude with respect to initial value in the presence of gas concentrations up to few ppm in air at ambient pressure (Raut *et al.*, 2013).

In this study, ultrasonic nebulizer method was used for fabricating CdS thin films, the purpose of this research was to investigate the effect of film thickness on structural, optical and gas sensing properties of CdS thin film.

MATERIALS AND METHODS

Experimental details: Cadmium sulfide films were deposited onto preheated glass slides (430°C) with different thickness by Ultrasonic Nebulizer Deposition (UND) technique. Cadmium Chloride salt ($\text{CdCl}_2 \cdot 2\text{H}_2\text{O}$, 234.644 g/mol (99.98%) pure BDH Chemical Ltd Pool England) and thiourea ($\text{CS}(\text{NH}_2)_2$, 76.12 g/mol, 99% pure, BDH Chemical Ltd Pool England) were dissolved in distilled water. The precursor solution of cadmium sulfide films was prepared by mixed aqueous solution (1:1) of cadmium chloride salt (0.2 M) and aqueous solution of thiourea (0.2 M) to make a 0.2 M solution of total metal content. The resulting solution was sprayed onto heated glass substrates using an ultrasonic nebulizer system (Sonics) which transformed the liquid to a steam. In order to get good quality films and complete combustion all the deposition parameters

such as the distance between the substrate and the nozzle, gas flow rate, deposition temperature and the concentration of the solutions were optimized.

Film thickness (t) measured by weight difference method and optical interferometer method. The optical method was based on interference of He-Ne laser light beam reflected from film surface and substrate bottom by using the known Eq. 1:

$$t = \frac{\Delta x}{x} \times \frac{\lambda}{2} \quad (1)$$

Where:

- x = The fringe width
- Δx = The distance between two fringes
- λ = The wavelength of laser light (632.8 nm)

The structural properties of the films were characterized by X-Ray Diffraction (XRD) using Philips PW 1840 diffractometer with Cu K α radiation ($\lambda = 1.5406$ Å) operated at 40 kV and 30 mA. All samples were scanned in the range (20-70°) with a scan speed of 5°/min. Surface studies of the samples were done with the help of

Atomic Force Microscopy (AFM) type (SPM-AA3000 contact mode spectrometer, Angstrom). Optical transmission and absorption spectra of the films were recorded in the wavelength range of (370-1100 nm) using UV-VIS-NIR spectrophotometer (type Shimadzu).

The gas sensing properties of the films at different concentration (10-30 ppm) of ethanol were evaluated at various operating temperatures in the range of 70-400°C by measuring the changes of resistance of the films in air and in the gas ethanol. The resistance was measured using Keithley 6514 electrometer.

RESULTS AND DISCUSSION

Figure 1 shows, the X-ray diffraction patterns for CdS thin films deposited at 430°C with different thicknesses (300-600 nm). From Fig. 1 it can be seen that all films show the diffraction peaks from (100), (002), (101), (102), (110), (103), (112) planes which correspond to hexagonal structure of polycrystalline CdS. No diffraction peaks from other impurities were found, indicating the high purity of the samples. Also, it can be seen that the

Fig. 1: XRD of CdS thin films at different thickness: a) CdS 300 nm; b) CdS 400 nm; c) CdS 500 nm and d) CdS 600 nm

(101) diffraction peak is predominate in thickness (300 and 400 nm). However as the film thickness increased (500 and 600 nm) the (002) diffraction peak is predominant, this means that the c-axis of the CdS films changed from inclined to the substrate to perpendicular to the substrate. These results imply that the mechanism of preferred orientation development changed with increasing thickness.

The values of lattice constants a and c are calculated using Eq. 1) and listed in Table 1, the result showed that the all values are agreement with standard JCPDS card No. 41-1049 (Macleod, 2001).

Table 1: Structural parameters of CdS films from ray diffraction measurements

Sample thickness (nm)/(hkl)	d(Å)	Lattice		
		a _o	c _o	G (nm)
300				
(002)	3.35661	4.131	6.72	50.67
(101)	3.15754			
(100)	3.57727			
400				
(002)	3.35292	4.130	6.705	27.35
(101)	3.15754			
(100)	3.57834			
500				
(002)	3.35524	4.143	6.713	35.55
(101)	3.15914			
(100)	3.57834			
600				
(002)	3.34821	4.126	6.694	56.68
(101)	3.15287			
(100)	3.57098			

$$\frac{1}{d^2} = \frac{4}{3} \left(\frac{h^2 + hk + k^2}{a^2} \right) + \frac{l^2}{c^2} \quad (1)$$

The crystallite size (G) of the films calculated from the highest peak using the following relation (Debye-Scherer formula) (Hazaa, 2015):

$$G = \frac{0.9\lambda}{\beta \cos \theta} \quad (2)$$

Where:

- = The wavelength of X-rays which is = 1.5406 Å
- = The Full Width at Half Maximum (FWHM) measured in radians
- = The Bragg angle

Atomic Force Microscopy (AFM): Figure 2 shown the images (AFM) of CdS thin films for different thickness on the glass substrate at temperature (430°C), Table 2 shown the Root Mean Square (RMS), roughness and grain size different with films thickness. The grain size range values between (56.68-84.12 nm) these values indicate of increase surface roughness comfort into increase the size of all crystalline (Sagar *et al.*, 2005).

Table 2: The result from the AFM of CdS different thickness

Sample thickness (nm)	Roughness (nm)	RMS (nm)	Grain size (nm)
300	17.4	19.8	63.42
400	14.2	16.6	74.47
500	10.4	12.3	56.68
600	10.5	13.6	84.12

Fig. 2: AFM images for CdS films at different thickness: a) t = 300 nm; b) t = 400 nm; c) t = 500 nm and d) t = 600 nm

Fig. 3: Transmittance as a function of wavelength at different thickness (CdS)

Fig. 4: Absorbance as a function of wavelength at different thickness (CdS)

Optical properties: The optical properties of all films with different thicknesses (300–600 nm) have been determined by using Transmittance (T) and Absorbance (A) spectrum in the region (370–1100 nm). Figure 3 and 4 show, that the transparency decreases and absorbance increases as the thickness increase may due to thickness or to absorption coefficient. The absorption coefficient (α) which is a function of the photon energy ($h\nu$) is calculated from the optical transmittance spectra results using the following Eq. 4 (Al-Hamdani and Salih, 2012):

$$\alpha = (1/t) \ln(1/T) \quad (4)$$

All the films as shown in Fig. 5 had high absorption coefficient ($>10^5 \text{ cm}^{-1}$) above the fundamental absorption edge, indicates the existence allowed transitions and the absorption coefficient increase as the thickness increase. The optical band gap was calculated using following (Cheng and Conibeer, 2011):

$$\alpha h\nu = B(h\nu - E_g)^r \quad (5)$$

Fig. 5: Absorption coefficient as a function of wavelength at different thickness (CdS)

Table 3: Optical band gap for CdS films with different thickness

Thickness (nm)	E_g (eV)
300	2.35
400	2.40
500	2.38
600	2.42

Where:

$h\nu$ = The photon energy

E_g = The optical band gap

B = A constant

r = The 1/2, 3/2, 2 or 3 for direct allowed, direct forbidden, indirect allowed and indirect forbidden transitions, respectively

A satisfactory linear fit is obtained for $(\alpha h\nu)^2$ vs. $h\nu$, indicating the presence of direct allowed transition for thin films. The intercept on the energy axis as shown in Fig. 6, give the optical band gap E_g of the material and listed in Table 2 which are related to the variation of films structures. These values of optical band gap are comparable with the reported value for CdS thin films (Khallaf *et al.*, 2008; Mona, 2010; Hasnat and Podder, 2013) (Table 3).

Figure 7 and 8 show, the resistance variation with operating temperature of CdS films for different thickness in air and in ethanol gas, respectively. There is a decrease in resistance with increase in temperature indicating semiconducting behavior and the resistance of CdS film samples upon exposure to ethanol gas was lower than that in air because reduction nature of ethanol gas which is attributed to the decrease in potential barrier at grain boundaries, this result is agreement with other (Raut *et al.*, 2013). The Sensitivity (S) of the sensor toward ethanol gas was measured by using the following relation (Al-Janaby and Al-Jumaili, 2016).

$$S = \frac{R_a - R_g}{R_a} \times 100\% \quad (6)$$

Fig. 6: $(\alpha \cdot h\nu)^2$ vs. photon energy for CdS films with different thickness: a) $t = 300$ nm; b) $t = 400$ nm; c) $t = 500$ nm and d) $t = 600$ nm

Fig. 7: Resistance vs. operating temperature in air

Fig. 8: Resistance vs. operating temperature in 20 ppm ethanol

Fig. 9: Sensitivity vs. operating temperature for 20 ppm ethanol

Where:

R_a = The Resistance of the film in air

R_g = The Resistance of film upon exposure to ethanol

Figure 9 and 10 shows the sensitivity as functions of operation temperature CdS thin films exposed to 20 ppm ethanol gas concentration with noble metal with different film thickness. For all the samples the sensitivity increases with increase in operating temperature and reach maximum ($S = 75$ for sample with thickness 500 nm) at 310°C .

Fig. 10: Sensitivity vs. operating temperature with different ethanol concentration ($t = 500 \text{ nm}$)

Response of sensors depends on two factors, the speed of chemical reaction on the surface of the grains, the speed of the diffusion of gas molecules to that surface. At low temperatures the sensor response is restricted by the speed of chemical reactions. At higher temperature the sensor response is restricted by the speed of the diffusion of gas molecules to that surface. At some intermediate temperature the speed values of two processes become equal and at that point the sensor response reaches its maximum. According to this mechanism for every gas there is a specific temperature at which the sensor response attains its peak value (Ramesh *et al.*, 2014).

The response time of the sensor is usually defined as the time taken to achieve at least 90% of the final change in its sensitivity during exposure to the tested gas. While the recovery time is generally, defined as the time taken by the sensor to get back at least 90% of its original state after exposure to air by maintaining the operating temperature constant (Dhahri *et al.*, 2017).

The variation of the sensitivity with time of CdS sensors (thickness 500 nm) at 310°C after exposure to 20 ppm ethanol gas is shown in Fig. 11. It was found that the response time was 11 sec while recovery time was 20 sec .

It was observed from Fig. 12 that the response times and recovery times depended on the operating temperature. Both the response times and recovery times were found to shorten at higher operating temperatures. This is may be due to the fact that at higher temperature, the speed of the surface reaction increases because of sufficient thermal energy of the sensor material. However, the response time was found to be shorter than the

Fig. 11: Sensitivity with response time and recovery time of CdS (CdS 20 ppm ethanol at 310°C)

Fig. 12: Dependence of response and recovery time on operating temperature (20 ppm)

recovery time at all operating temperature. In this research, the response time and recovery time were found to be 10 and 15 sec , respectively at 400°C higher operating temperature.

CONCLUSION

CdS thin films with various thickness was grown successfully via. Ultrasonic Nebulizer Deposition (UND) technique. All films represented hexagonal structure of polycrystalline CdS with the band gap values of $2.35\text{--}2.42 \text{ eV}$. The optimum film thickness and operating temperatures are found to be 500 nm and 310°C , respectively and with fast response and recovery time were found to be 10 and 15 sec , respectively, at 400°C operating temperature.

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