

Recital Exploration of Enclosure of Hydrogen to Compression Ignition Diesel Engine with Biodiesel Mingles

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Abstract: The objective of reducing the discharge of Nitrogen Oxide (NO_x) in CI engine through mingled bio fuel is a operative unconventional fuel for fossil fuels in provisions of contamination decrease in discharge and effectiveness augmented in engine. The performance and discharge features of a CI engine and the updraft efficacy amplified by influence of hydrogen through bio fuel are deliberate in this exploration. The stability of ignition by accumulation of hydrogen and the effectiveness of NO_x decrease correspondingly engaged by means of HGBD as an fuel.

Key words: CI engine, thermal efficiency, emission, Hydrogen and Bio Diesel blends (HGBD), performance, India

INTRODUCTION

An internal combustion engine is an obligatory and critical part of everyday life. Though, diesel engines produce conspicuous such as impulsive and recurrent noises which are unpleasant (Alt *et al.*, 2005). Combustion blare possibly will be reformed by using another type of fuel. Hydrogen is the largest part of potential fuels because it has dirt free burning characteristics and healthier performance matched up to other fuels. Though, hydrogen cannot be used as the solitary fuel in a CI engine because the compression temperature is not enough to kick off combustion due to its elevated self-ignition temperature (Maxwell, 1892). The observed recompenses of this are largely reduced CO discharges, HC and PM then through eventually amplified NO_x discharges associated to fossil diesel fuels. That's why an ignition source is obligatory whilst using it in a CI engine.

The easiest method of utilizing hydrogen in a CI engine is to run in the dual fuel mode in the company of diesel fuel that be capable of perform as an explosion cause for hydrogen. Various inquiries already defined on the co-ignition of hydrogen-diesel combustible mixtures (Das, 2002). Miyamoto *et al.* (2011) investigated the production features of the diesel engine with hydrogen added to the absorption air at deferred inoculation timings. That has inspected the retort of diesel-fuel inoculation scheduling on the extreme ratio of in-chamber compression increase aimed at a diesel engine through

accumulation of hydrogen to the absorption air (Jacobs, 1963). The outcome validated in the event of a diesel-fuel inoculation consequently TDC through accumulation of 11 vol% hydrogen to the absorption air, the elevated percentage of in-chamber density increase was reasonably lesser than that without hydrogen accumulation at higher heaps for a unsurprisingly trailed diesel engine. Hydrogen is essentially the finest swearing alternative fuels. Hydrogen combustion essentially not produces CO₂ and smoke, meanwhile that designated as a carbon-free fuel. Eason *et al.* (1995) showing that hydrogen fueled CI engine with fuel outflow from the injector could sustenance combustion of the hydrogen fuel. While burned in IC engines, hydrogen has been acknowledged as an on-spot carbon free energy carter with admirable ignition features. Delectable ignition possession such as a profligate flame proliferation speed and extensive slender effective variety make H₂ an eminent fuel for SI engines (Furuhama, 1983). By blending H₂ possessed by the ingestion mingle, hydrogen be capable of flamed in CI engines. The compressed H₂-air mingle is kindled by an experimental diesel sprig as the compression stroke finished. An effectual and consistent methodology to tingle numerous sparkling fuels such as H₂ in CI engines, dual fuel process has been endorsed (Gopal *et al.*, 1982). Numerous investigates narrated the pros and penalties accompanying with the change-over of environment diesel by H₂. These encompass the augmentation to the BTE, NO_x discharge augment, impeding the jerk of combustion, refining the heat

discharge practice and currently the on-spot discharge diminution of Carbon dioxide (CO₂). The formerly finished investigation procedure on H₂-diesel mingled dual fuel engines was accomplished through diffident single cylinder diesel engines such as the experimentation specified by Varde and Frame (1983).

A cram on the properties of hydrogen addition to precise biodiesel was initiated by Bika *et al.* (2008). In recent times, diverse investigators founded the possessions of H₂ accumulation on the recital as well as the ignition uniqueness of multi-cylinder; fewer purpose diesel engines (Karim, 2003a, b). The addition of H₂ to these less function diesel engines was considered to augment significantly the discharges of NO₂ conveyed with a lessening in NO discharges. For instance, Shirk *et al.* (2008) examined the possessions of H₂ accumulation on the exhaust discharges of a 1.3 L, turbocharged, light-duty diesel engine. The accumulation of H₂ somewhat abridged the discharges of NOx whereas its significance on the BTE was discreetly small. The dissever must generate these modules; reintegrating the applicable criteria that follow. Hydrogen has been injected to CI engine. Meanwhile, hydrogen has been injected to dual-fuel category diesel engines in which diesel-fuel combustion is burning basis for hydrogen (McWilliam *et al.*, 2008). This investigates concentrated hydrogen to absorption air while the diesel fuel was ingested straightly hooked on the chamber.

NOx emission mechanism

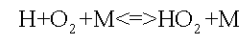
Impression of hydrogen accumulation on ignition: The NOx emissions of combustion devices burning fuels that are Nitrogen (N) free can be designed through the underneath contrivances) NOx updraft contrivance conquered by the native hotness of the burning yields) the rapid NOx contrivance detected primarily at fuel amusing blend and unburned fuel-air assortment preceding to the influx of the fore-flame and) the N₂O intermediate mechanism occurring mainly at trifling heap procedure of diesel engines and gas turbines (Miller and Bowman, 1989). When operated under medium to high load, the local combustion temperature of a diesel engine is usually higher than the threshold temperature for the development of NOx through NOx thermal mechanism. Comparatively, the N₂O transitional contrivance persuaded to subsidize suggestively to NOx development in diesel engines and gas turbines at lesser heap maneuver where the engine-out NO₂/NOx ratio is known to exceed 10% (Sahoo *et al.*, 2009).

Among these, the contribution of the prompt mechanism to the development of NOx in diesel fuelled engines is moderately trivial. The development contrivance of NO₂ has been researched by various

researchers (Saravanan and Nagarajan, 2008). It was noticed that the Nitrogen oxide molded in the blaze section could be rehabilitated to NO₂ through responses such as:



Past research reported the salient role of HO₂ in potentiating the alteration of NO to NO₂. The HO₂ portion of a particle can be designed by another reaction:



Procedures devouring the impeding to noticeably increase the deliberation of HO₂ were expected to encompass the development of NO₂. For example, the HO₂ portion of a particle systematized in the moderately less warmth unburned blend area preceding to the fore flame. The HO₂ enrich mingle reacts with the NO particles conveyed through high temperature ignition areas and augments the development of NO₂. When available at a appropriate heat, the unburned fuels contusing hydrogen could oxidize in the occurrence of O₂ and outline HO₂ which might augment the progress of NO₂. This might help to describe the significant enhancing property on the development of NO₂ when H₂ was blended into the ingestion mixture of diesel engines as reported in the literature (Sellerbeck *et al.*, 2007; Varde and Frame, 1983) investigated a processing of decreased diesel matter in the exhaust by articulating less quantities of gaseous hydrogen in the ingestion of a diesel engine. The outcome demonstrates that smoke reduced with the prolonged hydrogen accumulation. However, NOx and ignition disturbance augmented since fine ignition happened as an outcome of elevated combustion enhance of hydrogen.

Lilik *et al.* (2010) uttered that dual-mingle fuel procedure of rubber seed oil and its mingle through hydrogen. The consequences describe that NOx discharge augmented with the prolonged hydrogen energy fraction for RSO and ROME. Turns (2000) suggested a double fuelled engine with hydrogen and diesel-fuel under the PPCI (Premixed Power Compression Ignition) circumstance. Hydrogen was provided to the absorption port and diesel fuel was conveyed directly into the combustion cylinder. The diesel-fuel was assorted systematically with hydrogen-air mingle and combustion turn into mild as preminent diesel fuel inoculation effectiveness was sustained.

EGR is effective in diminishing NOx and evading colliding, though the smoke discharge augments along EGR in traditional diesel engines. Therefore, EGR is controlled to a very trivial EGR rate. Smoke-less and NOx-less combustion was made successful by this

method and it is termed as low temperature combustion method (Kumar *et al.*, 2003). Smoke formation depends on combustion high temperature and correspondence ratio.

Impact of hydrogen on biodiesel blends: Biodiesel is the popular utilized reusable fuel in CI engines. The better component of the researches accepts that PM, THC and carbon monoxide discharge from biodiesel are lesser to normal diesel fuel (White *et al.*, 2006). The oxygen content of biodiesel that stimulates an added whole and cleaner combustion process is the main factor (Yorozu *et al.*, 1987). The biodiesel usage could lead to more effective THC, CO and particulate matter oxidation and increased NOx emissions, depending on the engine technology employed, combustion characteristics and other physical and chemical properties of the biodiesel comparatively with nature diesel. The additional feature which justifies the PM reduction with revere to diesel is the nonexistence of pungent compounds in biodiesel (Das, 1990). The present study attempted to resolve the tradeoff between NOx and smoke under high load conditions without scarifying indicated thermal efficiency by LTC with hydrogen mixed to the ingestion mixture for the delayed diesel-fuel injection timing in a high-pressure direct injection diesel engine. This study offers two approaches to LTC (Young, 1989). Study, the injection timing of diesel-fuel was deferred drastically until 2° ATDC or high to reduce combustion temperature for hydrogen concentration in ingestion mixture within the flammability choice. Subsequently, amplified EGR rate is done almost upto stoichiometric condition with little amount of hydrogen to decrease combustion temperature considerably.

MATERIALS AND METHODS

The experimental apparatus was lay down as detailed in Fig. 1. The engine was a single cylinder, naturally diligence research engine and engaged a pump-line-nozzle direct injection system as described in Table 1. To load the engine an eddy current dynamometer has been utilized. The Kistler pressure transducer was escalated at the cylinder head through charge amplifier to a data acquisition board to the in-cylinder pressure traces. The digital shaft encoder has been used to measure crank shaft position. Alternate engine test assemble instrumentation was used to observe ingestion air, exhaust gas recirculation, temperatures (oil, air, inlet manifold and exhaust) and pressures. Data acquirement and combustion investigation were conceded out using a personalized lab view based code. A Horiba Mex an analyzer was engaged to determine the concentrations of gaseous emissions.

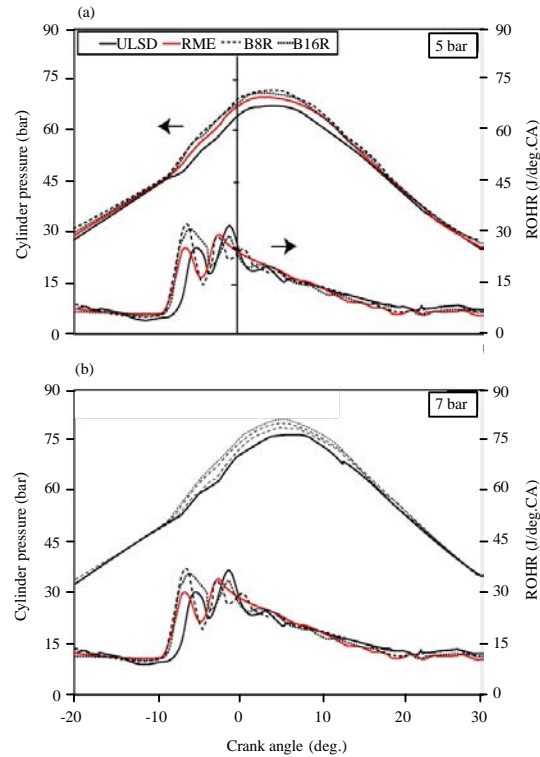


Fig. 1: In cylinder pressure and rate of heat release for the tested liquid fuels: a) 5 bar and b) 7 bar

Table 1: Engine specification

Engine specification	Values
Number of cylinders	1
Bore (mm)	98.4
Stroke (mm)	101.6
Connecting rod length (mm)	165
Displacement volume (cm ³)	773
Maximum torque (Nm)@1800 rpm	39.2
Maximum power (kW)@2500 rpm	836
Compression ratio	15.5:1
Injection timing (obTDC)	22
Maximum injection pressure (bar)	180
Injection system	Three holes pump-line-nozzle
Engine piston	Bowl-in-piston

A non-dispersive infrared, flame ionization detector and chemiluminescence method were employed to determine CO, THC and NOx correspondingly. To revise extent distribution of particulate matter emitted from the engine, a SMPS, fitted with thermo diluter was fitted. Experiments were carried out at a constant engine speed of 1500 rpm and changeable engine loads of 7 and 9 bar indicated mean effective pressure, representing 40% low and 70% high of ultimate load, respectively. The tests were processed out initially using diesel and biodiesel fuels as a instance. B8R and B16R blends were prepared and tested under the same conditions for comparison. Hydrogen mixed with the air before the ingestion manifold valve.

Table 2: Specification of tested fuels

Properties	ULSD	RME	Butanol	Hydrogen	B8R	B16R
Chemical formula	C ₁₄ H _{26.09}	C _{18.96} H _{35.29} O ₂	C ₄ H ₉ OH	H ₂	C _{15.36} H _{29.2} O _{1.76}	C _{12.83} H _{24.92} O _{1.59}
Cetane number	53.9	54.7	17	-	-	-
Density at 15°C (kg/m ³)	827.1	883.7	809.5	0.08	878.3	870.5
Kinematic viscosity at 40°C (cSt)	2.70	4.53	2.23	-	3.95	3.78
Lower heating value (MJ/kg)	43.11	37.80	33.12	120	37.12	36.91
Latent heat of vaporisation (kJ/kg)	243	216	585	-	-	-
Bulk modulus (MPa)	1410	1553	1500	-	-	-
Lubricity at 60°C (µm)	312	205	620	-	257	293
Stoichiometric A/F mass ratio	14.53	12.49	11.14	34.07	12.39	12.29
Sulphur (mg/kg)	46	5	-	-	-	-
Total aromatics (wt.%)	24.4	-	-	-	-	-
C (wt.%)	86.44	77.09	64.78	0	76.18	75.26
H (wt.%)	13.56	12.07	13.63	100	12.19	12.30
O (wt.%)	0	10.84	21.59	0	11.63	12.44

Abbreviations: Volumetric make-up (%); ULSD: 100 Ultra Low Sulphur Diesel; RME: 100 Rapeseed Methyl Ester; B8R: 8 Butanol+92 RME; B16R: 16 Butanol+84 RME

The property of hydrogen concentration (1, 1.5 and 2% of volumetric air flow rate) was estimated with the aim of resolving the optimal hydrogen concentration. Hence, the varied conditions of reticent EGR rate (5, 15 and 18%) were assessed to overcome the NOx penalty. The basic properties of tested fuels are given in Table 2.

RESULTS AND DISCUSSION

To achieve improved efficiency and emissions using lean burn combustion, it is essential to protected combustion stability in the lean operation condition such that the stable lean burn range is extended. Wobbly slant operation will source deterioration in competence and an augment of unburned hydrocarbon emissions. The NOx reduction, also is in adequate through the slender flammability edge. As noticed in preceding research and in this revise, there as on of accretion of hydrogen to a natural gas engine is to take benefit of the wider lean burn uniqueness of hydrogen. In this explore, the slant burn characteristics were processed according to the hydrogen addition ratio as the hydrogen addition was assorted from 10-40 vol.%.

The covalence values in Fig. 1 explain changes in combustion constancy with the hydrogen count proportion in the fuel at the MBT spark timing of each operation condition. If the covalence value is set as 2% as the typical for an operable stable combustion, it is pragmatic that the flammability edge is absolute by the hydrogen addition. Figure 2 demonstrates the thermal effectiveness against excess air ratio as hydrogen was supplemented. As the leanness was augmented, the thermal effectiveness enlarged, however, when the excess air ratio exceeded a certain level of leanness, the degree of efficiency decreased due to the degradation in combustion stability.

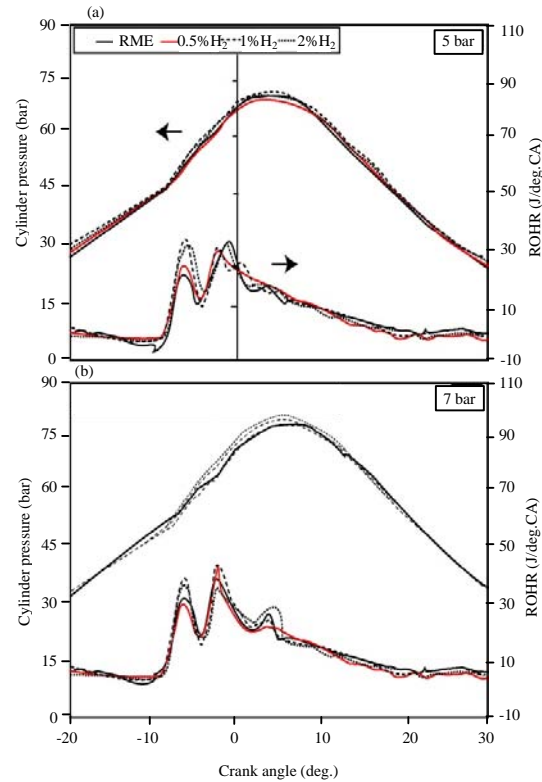


Fig. 2: The effect of hydrogen on the combustion characteristics of RME: a) 5 bar and b) 7 bar

The additional air ratio of maximum efficiency for each hydrogen addition proportion also denotes a leaner condition with the increase of the hydrogen addition proportion. It is prominent that the thermal effectiveness of 35 vol.% hydrogen addition was immensely less by 1.5%, than that of the natural gas.

The justification behind hydrogen addition at specific excess air proportions was reliable in amending thermal effectiveness is the efficient augmented work in order to

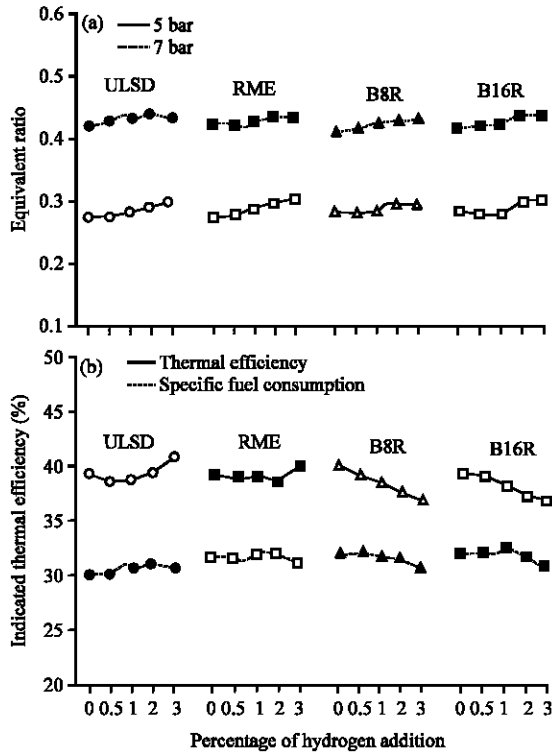


Fig. 3: Engine performance: a) Equivalence ratio and b) Indicated fuel consumption and indicated thermal efficiency

the increased laminar flame speed of the mixture as concluded in Fig. 3 which presents the MBT spark advance timing at each operating condition. An expansion of thermal effectiveness is presumed with an increase of the hydrogen addition proportion due to the anti-knocking characteristics of hydrogen are advantageous to form a increased compression proportion possible as higher hydrogen is mixed (Lilik *et al.*, 2010; McWilliam *et al.*, 2008; Miller and Bowman, 1989). Figure 3 shows the results of the dangerous emissions NO_x, CO₂ and CO, respectively as a measure of changes in the excess air proportion under the same operating condition as in Fig. 3.

As shown in Fig. 3 enlarged ratio for enhanced elucidate assessment, beneath certain surplus air quantity circumstances, the intensity of NO_x greater than before as hydrogen was assorted. This is due to promoted NO_x generation as the high adiabatic flame temperature of hydrogen extends the temperature of the combustion gas. Also, considering the best efficiency illustrated in Fig. 3, NO_x emissions are possibly to decrease because of possible stable operation of hydrogen addition with higher excess air proportion conditions.

A comparison of NO_x emissions with standard gas with the conditions of finest efficiency indicated as 64%

reduction of the NO_x with the addition of 35 vol.% hydrogen and 78% NO_x reduction with 35 vol.% hydrogen. The characteristics of CO emissions are actually slight different from that of NO_x emissions as shown in Fig. 3. CO emissions decreased with hydrogen addition at certain excess air proportion conditions, CO emissions are matching or higher at the operating condition of finest efficiency.

CONCLUSION

An analysis to attain NO_x reduction was achieved in a heavy duty natural gas engine with the addition of hydrogen to biodiesel blend fuel. As such to endorse the suitability of hydrogen-blended fuel, the thermal effectiveness and emission characteristics were reviewed. Therefore, recital and incineration aspect of a CI engine and the thermal competence augmented by persuade of hydrogen through bio fuel is scrutinized in this study. The reliability of ignition by accumulation of hydrogen and the competence of NO_x lessening as well unremitting by means of hydrogen gas mingled diesel as a fuel.

REFERENCES

- Alt, N., H.D. Sonntag, S. Heuer and R. Thiele, 2005. Diesel engine cold start noise improvement. SAE International, Warrendale, Pennsylvania, Troy, Michigan. <http://papers.sae.org/2005-01-2490/>.
- Bika, A.S., L.M. Franklin and D.B. Kittelson, 2008. Emissions effects of hydrogen as a supplemental fuel with diesel and biodiesel. SAE. Intl. J. Fuels Lubr., 1: 283-292.
- Das, L.M., 1990. Hydrogen engines: A view of the past and a look into the future. Intl. J. Hydrogen Energy, 15: 425-443.
- Das, L.M., 2002. Near term introduction of hydrogen engines for automotive and agricultural application. Intl. J. Hydrogen Energy, 27: 479-487.
- Eason, G., B. Noble and I.N. Sneddon, 1955. On certain integrals of Lipschitz-Hankel type involving products of Bessel functions. Philos. Trans. R. Soc. London, 247: 529-551.
- Furuhama, S., 1983. State of the art and future trends in hydrogenfueled engine. Intl. J. Veh. Des., 4: 359-385.
- Gopal, G., P.S. Rao, K.V. Gopalakrishnan and B.S. Murthy, 1982. Use of hydrogen in dual fuel engines. Intl. J. Hydrogen Energy, 7: 267-272.
- Jacobs, I.S., 1963. Fine particles, thin films and exchange anisotropy. Magnetism, 3: 271-350.

- Karim, G.A., 2003. Combustion in gas fueled compression: Ignition engines of the dual fuel type. *Trans. Am. Soc. Mech. Eng. J. Eng. Gas Turbines Power*, 125: 827-836.
- Karim, G.A., 2003. Hydrogen as a spark ignition engine fuel. *Intl. J. Hydrogen Energy*, 28: 569-577.
- Kumar, M.S., A. Ramesh and B. Nagalingam, 2003. Use of hydrogen to enhance the performance of a vegetable oil fuelled compression ignition engine. *Intl. J. Hydrogen Energy*, 28: 1143-1154.
- Lilik, G.K., H. Zhang, J.M. Herreros, D.C. Haworth and A.L. Boehman, 2010. Hydrogen assisted diesel combustion. *Int. J. Hydrogen Energy*, 35: 4382-4398.
- Maxwell, J.C., 1892. *A Treatise on Electricity and Magnetism*. 3rd Edn., Clarendon Press, Oxford, England, Pages: 505.
- McWilliam, L., T. Megaritis and H. Zhao, 2008. Experimental investigation of the effects of combined hydrogen and diesel combustion on the emissions of a HSDI diesel engine. SAE International, Warrendale, Pennsylvania, Troy, Michigan. <http://papers.sae.org/2008-01-1787/>.
- Miller, A. and C.T. Bowman, 1989. Mechanism and modeling of nitrogen chemistry in combustion. *Progr. Energy Combust. Sci.*, 15: 287-288.
- Miyamoto, T., H. Hasegawa, M. Mikami, N. Kojima and H. Kabashima *et al.*, 2011. Effect of hydrogen addition to intake gas on combustion and exhaust emission characteristics of a diesel engine. *Intl. J. Hydrogen Energy*, 36: 13138-13149.
- Sahoo, B.B., N. Sahoo and U.K. Saha, 2009. Effect of engine parameters and type of gaseous fuel on the performance of dual-fuel gas diesel engines-A critical review. *Renewable Sustainable Energy Rev.*, 13: 1151-1184.
- Saravanan, N. and G. Nagarajan, 2008. An experimental investigation of hydrogen-enriched air induction in a diesel engine system. *Intl. J. Hydrogen Energy*, 33: 1769-1775.
- Sellerbeck, P., C. Nettelbeck, R. Heinrichs and T. Abels, 2007. Improving diesel sound quality on engine level and vehicle level a holistic approach. SAE International, Warrendale, Pennsylvania, Troy, Michigan. <http://papers.sae.org/2007-01-2372/>
- Shirk, M.G., T.P. McGuire, G.L. Neal and D.C. Haworth, 2008. Investigation of a hydrogen-assisted combustion system for a light-duty diesel vehicle. *Int. J. Hydrogen Energy*, 33: 7237-7244.
- Turns, S.R., 2000. *An Introduction to Combustion: Concepts and Applications*. 2nd Edn., McGraw-Hill International, New York, USA., ISBN-13: 9780072350449, Pages: 676.
- Varde, K.S. and G.A. Frame, 1983. Hydrogen aspiration in a direct injection type diesel engine its effects on smoke and other engine performance parameters. *Intl. J. Hydrogen Energy*, 8: 549-555.
- White, C.M., R.R. Steeper and A.E. Lutz, 2006. The hydrogen-fueled internal combustion engine: A technical review. *Int. J. Hydrogen Energy*, 31: 1292-1305.
- Yorozu, Y., M. Hirano, K. Oka and Y. Tagawa, 1987. Electron spectroscopy studies on magneto-optical media and plastic substrate interface. *IEEE Trans. J. Magn. Jpn.*, 2: 740-741.
- Young, M., 1989. *The Technical Writers Handbook*. University Science Books, Mill Valley, California.