

H^∞ and μ -Synthesis Design of Coupled Tanks Level Control

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Abstract: In this study, the design and analysis of coupled tank water level control system is done using robust control theory. The main aim of this work is to improve level controlling mechanisms in industries and household areas. In this study, H^∞ and μ -synthesis controllers are designed to improve the level control system. The coupled tank water level control system is designed using the proposed controller's comparison and tested for tracking a reference level signals (step, sine wave and random) and simulation results have been analyzed successfully. Finally, the comparative simulation results prove the effectiveness of the proposed coupled tank water level control system with H^∞ controller for improving the tracking mechanism performance of the system.

INTRODUCTION

Many in advance works dealt with various strategies of controlling of liquid level of coupled tanks in industrial and home packages. Broadly this manage problem can be completed underneath two method: mechanical methods and electrical methods^[1]. Float ball type liquid level control is a famous technique of control nevertheless utilized in practice for regular applications such as overhead tank overflow restrictors etc. The electrical techniques of control include a microcontroller-control based circuits which robotically expect the liquid level and for that reason active the circuit to perform the action. In spite of several such to be had techniques, still there are new techniques on this application so as keep away from dangerous working situations in commercial boilers.

MATERIALS AND METHODS

Mathematical model of the two tanks system: Figure 1 represents a two-tank liquid-level control system. Definitions of the system parameters are:

q_i, q_1, q_2 = Rates of flow of fluid
 h_1, h_2 = Heights of fluid level
 R_1, R_2 = Flow resistance
 A_1, A_2 = Cross-sectional tank areas

The following basic linear relationships hold for this system:

$$q = \frac{h}{R} = \text{rate of flow through orifice} \quad (1)$$

$$q_n = (\text{tan k input rate flow}) - (\text{tan k output rate flow}) = \text{net tan k rate flow} = ADh \quad (2)$$

Applying Eq. 2 to tanks 1 and 2, respectively yields:

$$q_{n1} = A_1 Dh_1 = q_i - q_1 = q_i - \frac{h_1 - h_2}{R_1} \quad (3)$$

$$q_{n2} = A_2 Dh_2 = q_1 - q_2 = \frac{h_1 - h_2}{R_1} - \frac{h_2}{R_2} \quad (4)$$

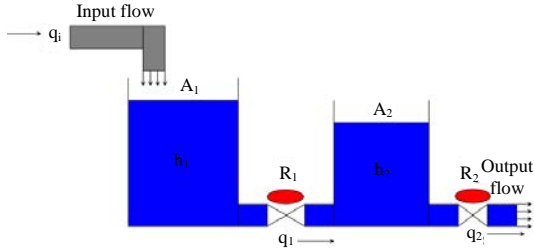


Fig. 1: Two-tank liquid-level control system

Table 1: Parameters of the tank

Parameters	Symbols	Values
Area 1	A_1	2.4 m ²
Area 2	A_2	1.8 m ²
Resistance 1	R_1	0.4 s/m ²
Resistance 2	R_2	0.7 s/m ²

Letting $x_1 = h_1$, $x_2 = h_2$, and $u = q_i$ in Eq. 3 and 4 reveals that x_1 and x_2 are independent state variables. Thus, the state equation is:

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix} = \begin{pmatrix} -\frac{1}{R_1 A_1} & \frac{1}{R_1 A_1} \\ \frac{1}{R_1 A_2} & -\frac{1}{R_1 A_2} - \frac{1}{R_2 A_2} \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} + \begin{pmatrix} \frac{1}{A_1} \\ 0 \end{pmatrix} u \quad (5)$$

The levels of the two tanks are the outputs of the system. Letting $y_1 = x_1 = h_1$ and $y_2 = x_2 = h_2$ yields:

$$y = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} x \quad (6)$$

The parameters of the tank is shown in Table 1:

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix} = \begin{pmatrix} -1.0417 & 1.0417 \\ 1.39 & -2.184 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} + \begin{pmatrix} 0.42 \\ 0 \end{pmatrix} u$$

$$y = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} x$$

Weighting functions: It is required that within the H^∞ framework to use weighting functions to reconciliation distinct overall performance targets. The performance aim of a comments system may be normally determined in phrases of requirements at the sensitivity features and/or complementary sensitivity features or in phrases of some other closed loop transfer functions^[2]. The odds of occupying weighted overall performance in multivariable system design is firstly, some part of a vector signal are generally more essential than others, secondly, measuring each signal will not be inside the equal unit. For instance, a few part of the output error signal can be measured in terms of period and others may be measured in phrases of

voltage. Therefore, weighting functions play a vital rule to kind those component similar. The weighting functions are mentioned beneath.

W_{h_1} and W_{h_2} are used to keep the water level of the tank small over the desired range. The water level W_{h_1} is given as:

$$W_{h_1} = \frac{1}{s+5}$$

The water level h_2 is used via weighting function W_{h_2} . The weighting function is given as:

$$W_{h_2} = \frac{5}{0.2s+10}$$

The proposed controller design: The design of water level of the tank system to provide level control is evolved the use of H^∞ and μ -synthesis controllers design. In the water level of the tank system, the proposed controllers design to control the level of the water within the two tanks^[3]. The predominant purpose of the controller design is to decrease the error of the level of the two tanks. Synthesis method is used to design the proposed controllers through reaching the overall performance objective through minimizing the weighted transfer characteristic norm. The water level of the tank system with H^∞ and μ -synthesis controllers system interconnections block diagram for tracking level h_1 and level h_2 is shown in Fig. 2 and 3, respectively.

A μ -synthesis controller is synthesized the usage of D-K iteration. The D-K iteration method is an approximation to synthesis that tries to synthesize the controller. There is one manipulate input the desired level signal. There are two purposes for the weighted functions norm: for a given norm, there will be a direct evaluation for extraordinary performance targets and they are used for understanding the frequency data incorporated into the analysis. The output or feedback signal y is:

$$y = (h_{1,2} + d_1 \times W_n)$$

The controller's acts on the y signal to produce the feedback level signal. The W_n block modelled the disturbance inside the channel. W_n is given a disturbance noise of 0.05 m.

$$W_n = 0.05$$

W_n is used to model the noise of the level sensor. The magnitude of the level disturbance is scaled using the weight $W_{h_{ref}}$. Let us assume the maximum level disturbance is 0.15 m which means:

$$W_{h_{ref}} = 0.15$$

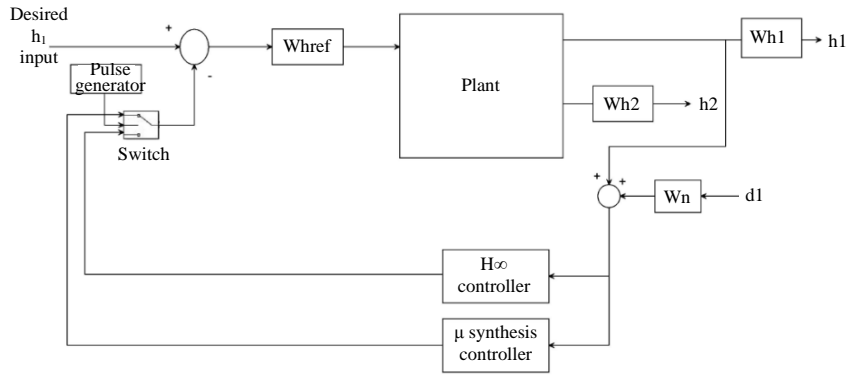


Fig. 2: Water level of the tank system with H^∞ and μ -synthesis controllers system interconnections block diagram for tracking level h_1

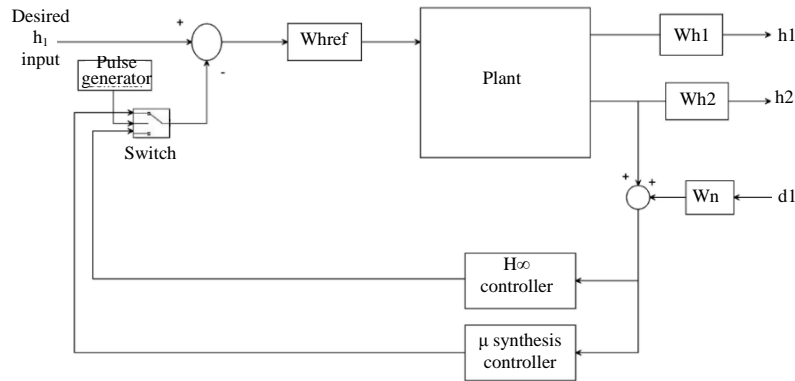


Fig. 3: Water level of the tank system with H^∞ and μ -synthesis controllers system interconnections block diagram for tracking level h_2

RESULTS AND DISCUSSION

Comparison of the water level of the tank system with H^∞ and μ -synthesis controllers: In this subsection, we simulate the water level of the tank system with H^∞ controller and μ -synthesis controller for the tracking of desired level using step, sine wave and random desired input signals^[4].

Simulation of a desired level step signal: The simulation for a step input level signal is shown below. In this simulation, we simulate the water level of the tank system with H^∞ controller and μ -synthesis controller for the tracking of desired level signal.

The tracking of desired level signal simulation output is shown in Fig. 4 and 5, respectively for tracking of desired level h_1 and h_2 , respectively.

Simulation of a desired level sine wave signal: The simulation for a sine wave input level signal is shown below. In this simulation, we simulate the water

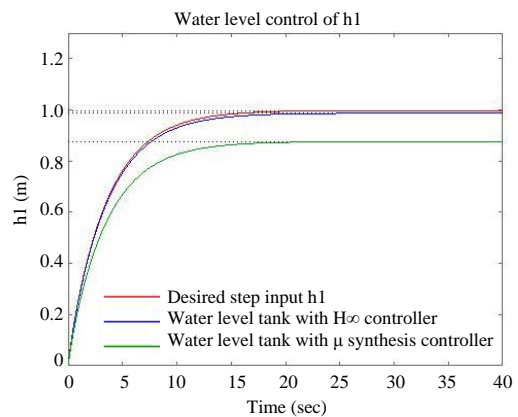


Fig. 4: Simulation of the actual and desired level for h_1

level of the tank system with H^∞ controller and μ -synthesis controller for the tracking of desired level signal. The tracking of desired level signal simulation output is shown in Fig. 6 and 7, respectively for tracking of desired level h_1 and h_2 , respectively^[5].

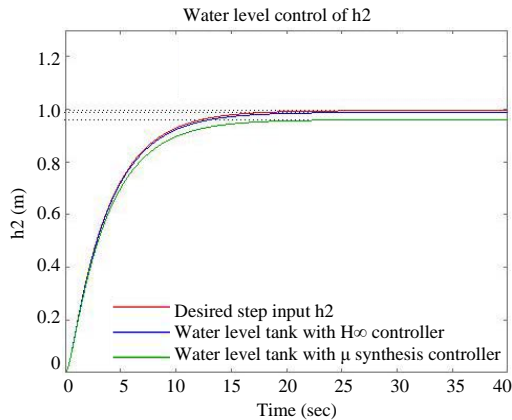


Fig. 5: Simulation of the actual and desired level for h2

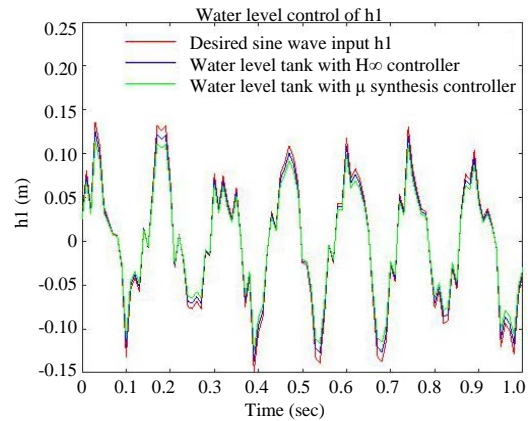


Fig. 8: Simulation of the actual and desired level for h1 (Wave of water level)

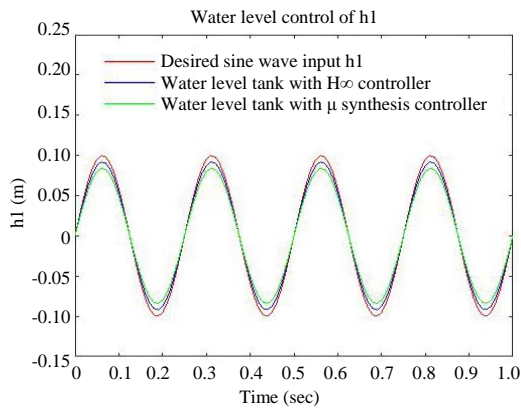


Fig. 6: Simulation of the actual and desired level for h1 (Signal simulation)

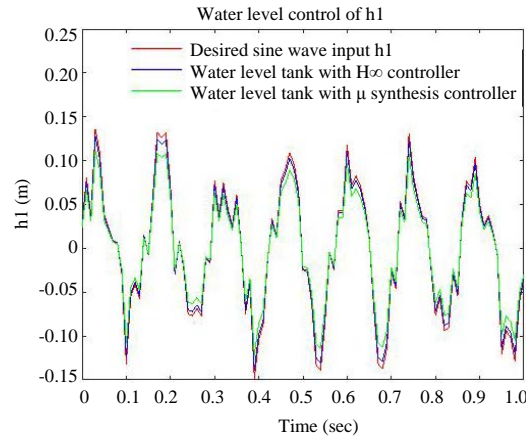


Fig. 9: Simulation of the actual and desired level for h2 (Desired of sine wave)

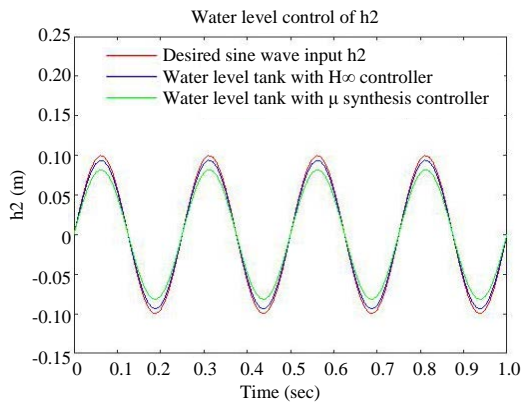


Fig. 7: Simulation of the actual and desired level for h2 (Sine wave)

Simulation of a desired level random signal: The simulation for a random input level signal is shown below. In this simulation, we simulate the water level of the tank system with H^∞ controller and μ -synthesis controller for the tracking of desired level signal.

The tracking of desired level signal simulation output is shown in Fig. 8 and 9, respectively for tracking of desired level h1 and h2, respectively.

Numerical values of the simulation outputs: The numerical values of the simulation output for the tracking of desired level using step, sine wave and random desired input signals is shown in Table 2-4.

Table 2 shows us the water level of the tank system with H^∞ controller have track the desired step input signal in the level h1 and h2 with good improvement than the water level of the tank system with μ -synthesis controller.

Table 3 shows us the water level of the tank system with H^∞ controller have track the desired step input signal in the level h1 and h2 with good improvement than the water level of the tank system with μ -synthesis controller.

Table 4 shows us the water level of the tank system with H^∞ controller have track the desired step

Table 2: Numerical steady state values of the desired step signal simulation output

Systems	h1 (m)	h2 (m)
Desired input signal	1	1
H^∞	0.99	1
μ -synthesis	0.87	0.92

Table 3: Numerical peak values of the desired sine wave signal simulation output

Systems	h1 (m)	h2 (m)
Desired input signal	0.1	0.1
H^∞	0.097	0.096
μ -synthesis	0.085	0.084

Table 4: Numerical peak values of the desired random signal simulation output

Systems	h1 (m)	h2 (m)
Desired input signal	0.14	0.14
H^∞	0.13	0.138
μ -synthesis	0.12	0.115

input signal in the level h1 and h2 with good improvement than the water level of the tank system with μ -synthesis controller^[6].

CONCLUSION

In this study, the coupled tank water level control system with H^∞ and μ -synthesis controllers is designed, controlled and analyzed with Matlab/Script toolbox and a fascinating results have been analyzed successfully. Comparison of the system with the proposed controllers is done for tracking a three reference level signals (step, sine wave and random) and the coupled tank water level

control system with H^∞ controller improve the tracking mechanism in the three reference input signals and shows that this system can be designed with robust controllers in industries and home appliances systems.

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