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Empirical Modeling of Surface Roughness in turning process of 1060 steel using Factorial Design Methodology

A. Doniavi, M. Eskandarzade and M. Tahmasebian Department of Mechanical Engineering, University of Urmia, Urmia, Iran

Abstract: Surface quality is of great importance for the functional behavior of mechanical parts. Surface roughness in addition to tolerances imposes one of the most critical constrains for cutting parameters selection in manufacturing process planning. Productivity for the finish turning can be improved by optimal selection of related parameters. The attempt of this study is to develop an imperial model with the use of response surface methodology that is widely adapted tool for the quality engineering field. The established predictive model shows that the feed rate was found to be main influencing factor on the surface roughness. It is increased with increasing the feed rate. But decrease with increasing cutting speed. The results for analysis of variance show that the first order term of depth of cut is not significant. But the first order term of cutting speed and feed rate are significant.

Key words: Surface roughness, response surface methodology, turning, cutting speed

INTRODUCTION

Cutting Process is a highly non linear phenomenon. There are many reasons, such as non-linear relations between stress and strain or stress and temperature or chemical kinetics and solid-state reactions in the material for non linearity in cutting process. Other sources involve nonlinear geometry such as contact forces or tool-work piece separation (Francis *et al.*, 2001).

The considerable research efforts have been devoted to study the non linear phenomena in machine-tool operations. Non-linear dynamics approach has employed by Marghitu et al. (2001) to analyze the interaction between cutting tool and disk work piece. The harmful vibrations called chatter may influence turning process and cause to poor surface quality and reduced dimensional accuracy of manufactured work piece. The method based on dynamics of cutting has proposed by Gradisek et al. (1998a) for chatter detection in turning on a lathe, the analysis of time series from stochastic process to examine whether the transition from chatter-free cutting to chatter resemble the Hopf bifurcation during cutting on a lathe have came in the investigation of Gradisek et al. (2002). With an increase of cutting depth the cutting regime is changed from chatter-free to chatter. Differences between these two cutting regimes (chatter-free cutting and cutting accompanied by chatter) have been described by Gradisek et al. (1998b) using non linear characteristics. Their research shows that chatter-free cutting is a

high-dimensional process, while the onset of chatter significantly alters the process dynamics, reduces dimensionality and increase the predictability of the process. Litak *et al.* (2004) has employed Fourier transform to experimental time series to investigate vibrations generated in a straight turning process.

Surface roughness is widely used as a quality index of manufacturing processes. Surface quality is of great importance for the functional behavior of mechanical parts (Şahin and Motorcu, 2004). It has been an important design feature and quality measure in many situations such as parts subject to fatigue loads, precision fits, fastener holes and esthetic requirements. Furthermore, surface roughness in addition to tolerances imposes one of the most critical constrains for cutting parameter selection in manufacturing process planning (Özel and Karpat, 2005). It is significantly affected by turning parameters. So by choosing effectively parameters and finding optimal points it can be improved productivity for the finish turning.

The attempt of this study is to develop an empirical model with the use of extracted experimental data. In this study to obtain our goals we used response surface methodology that is a widely adopted tool for the quality-engineering field. The response surface methodology comprises regression surface fitting to obtain approximate responses, design of experiments to obtain minimum variance of responses and optimizations using the approximated responses.

DESIGN OF EXPERIMENT

Experimental design is a critically important engineering tool for improving of process. Designed experiments can often be applied in the product design processes. This will produce information concerning which factors are most influential one and through use of this information the design can be improved.

The global form of the observed response is,

$$y_{ij} = \mu + \tau_i + \epsilon_{ij} \begin{cases} i=1,2,...,a \\ j=1,2,...,n \end{cases}$$
 (1)

Where y_{ij} is the (ij) the observation, μ is a parameter common to all factors called the overall mean, τ_i , is a parameter associated with the factor level called the (I)the factor effect and ϵ_{ij} is a random error component.

In design of experiment techniques, it is interested to test the equality of the a factor level means (Montgomery, 1996).

$$\begin{split} &H_0: \tau_1 = \tau_2 = ... = \tau_a = 0 \\ &H_1: \tau_i \neq 0 \qquad \text{for at least one } i \end{split} \tag{2}$$

That is, if the null hypothesis is true, then each observation is made up of the overall mean μ plus a realization of the random error ϵ_{ij} . The fundamental analysis of variance equation in test procedure for the hypotheses in Eq. 2 is,

$$\sum_{i=1}^{a}\sum_{j=1}^{n}(y_{ij}-\overline{y}_{..})^{2}=n\sum_{i=1}^{a}(\overline{y}_{i.}-\overline{y}_{..})^{2}+\sum_{i=1}^{a}\sum_{j=1}^{n}(y_{ij}-\overline{y}_{i})^{2} \quad (3)$$

Also, it can be written symbolically as,

$$SS_{T} = SS_{Factor} + SS_{E}$$
 (4)

Where, SS_T is the total sum of squares, SS_{Factor} is called the sum of squares due to the Factor and SS_E is called the sum of squares due to error.

If SS_{Factor} is large, it is due to differences among the means at the different factor levels. Thus, by comparing the magnitude of SS_{Factor} to SS_E it can be seen that how much variability is due to changing factor levels and how much is due to errors. This comparison leads to a statistical test based on F distribution for the equality of the factor means using the test static (Fairchild, 1998),

$$F_0 = \frac{MS_{Factor}}{MS_r} \tag{5}$$

Where, MS_{Factor} and MS_{E} are the Mean Square Error and Mean Square for Factor levels, respectively. They can be extract by dividing of SS_{Factor} and SS_{E} to there number of degrees of freedom.

If $F_0 \succ F_{\alpha,a-1,a(n-1)}$, we may conclude that the factor-level means are different.

One most important stage in using of DOE is selecting a suitable design. The designs can be full factorial, fractional factorial, Taguchy orthogonal arrays, Latin hyper cube, Box-Behnken, central composite and etc. choosing of an initial DOE is problem depend and is based on the number of independent variables in the model, the overall accuracy desired and the behavior of the response (Noordin *et al.*, 2004).

Where, there are many variables that are involved at process design and improvement, factorial experimental designs are the best choice. In this situation if the number of levels is limited in two ones, the great effectiveness can be achieved in industrial experimentation.

Surface quality in turning: Turning is a manufacturing process in which a work piece is held and rotated about its longitudinal axis on a machine tool called a lathe. Cutting tools mounted on the lathe are fed into the work piece to remove material and thus produce the required shape. The principal surfaces machined are concentric with the longitudinal axis of the work piece.

Surface finishes that can be maintained in turning vary depending upon the machine and operating parameters are used, the work piece, setup rigidity and other variables. Better smooth surface finishes can be produced particularly with precision machines and tools but several cuts are generally required, resulting in increased manufacturing costs.

Cutting speed in generally given in surface meters per minute (m min⁻¹), which is the rate at the work piece surface moves past the cutting tool. Feed rate is the rate at which the tool advances along its cutting path. It is expressed in millimeters per revolution (mm rev⁻¹). Depth of cut is the thickness of the layer of material removed from work piece surface, expressed in millimeters.

Turning conditions: After randomizing the rank orders with the use of Design of Expert Software, it provided work sheets and the experiments were done based on these work sheets. The lathe used for cutting tests equipped with spindle speed up to 2000 rpm. The cutting tools were coated carbide grade k10 inserts. And the material used in this research was AISI 1060 steel that was cut into bars with 20 mm diameter and 250 mm length. Table 1 show the cutting conditions have used.

Table 1: The cutting conditions

		Feed rate (mm rev ⁻¹)	Depth of cut (mm)	Coding				
Run	Cutting speed (m min ⁻¹)			X1	X2	X3	Response (µm)	
1	23	0.20	0.5	-1	1	-1	37.500	
2	34	0.15	1.0	0	0	0	31.000	
3	34	0.15	0.5	0	0	-1	24.375	
4	45	0.10	1.5	1	-1	1	14.625	
5	23	0.15	1.0	-1	0	0	28.125	
6	34	0.10	1.0	0	-1	0	16.250	
7	45	0.10	0.5	1	-1	-1	14.375	
8	45	0.20	1.5	1	1	1	32.500	
9	34	0.15	1.5	0	0	1	25.625	
10	45	0.15	1.0	1	0	0	22.500	
11	23	0.20	1.5	-1	1	1	41.250	
12	23	0.10	0.5	-1	-1	-1	16.875	
13	34	0.15	1.0	0	0	0	25.000	
14	34	0.15	1.0	0	0	0	23.000	
15	34	0.15	1.0	0	0	0	24.000	
16	34	0.15	1.0	0	0	0	25.250	
17	23	0.10	1.5	-1	-1	1	17.500	
18	34	0.20	1.0	0	1	0	35.000	
19	45	0.20	0.5	1	1	-1	32.500	
20	34	0.15	1.0	0	0	0	20.000	

Table 2: ANOVA table for response surface

	Sum of		Mean	F	p-value
Source	squares	df	square	value	prob>F
Model	1047.28	3	349.09	65.62	< 0.0001
A-cutting spread	61.26	1	61.26	11.51	0.0037
B-feed rate	982.58	1	982.58	184.70	< 0.0001
C-depth of cut	3.45	1	3.45	0.65	0.4324
Residual	85.12	16	5.32		
Lock of fit	19.57	11	1.78	0.14	0.9971^{NS}
Pure error	65.55	5	13.11		
Cor total	1132.40	19			

NS = Not Significant

ANOVA Analysis: The analysis of variance (ANOVA) was used to check the adequacy of the quadratic model. However, some errors typically results in this model from measurement error, the effects of variables not included in the experiment, variation due to chance causes in the process and so on (Onwubolu, 2005). Table 2 shows the ANOVA Table of response surface quadratic model for Surface roughness. The Model F-value of 65.62 implies the model is significant.

Values of Prob > F less than 0.0500 in Table 2 indicate that the model terms are significant. This is desirable as it indicates that the terms in the model have significant effect on the response. However, the first order term of Depth of Cut is not significant.

First-order model: Suppose that the response variable R_z , can be predicted as linear combination of independent variables such as cutting speed, feed rate and depth of cut as follows,

$$R_{z} = c_{0} + c_{1}.v + c_{2}.f + c_{3}.d$$
 (6)

Where; R_z is the surface roughness in μm , V is the cutting speed (m min⁻¹), f is the Feed rate (mm rev⁻¹), d is the depth of cut (mm), c_0 , c_1 , c_2 , c_3 are constants.

The regression analysis technique using least squares estimation was applied to compute the coefficients of the model for surface roughness (R_z) , the following model for a determined is given:

$$R_{z} = c_{0} + c_{1}v + c_{2}f + c_{3}d + c_{4}v^{2} + c_{5}f^{2} + c_{6}d^{2} + c_{7}vf + c_{8}vd + c_{9}fd$$
(7)

Second-order model: Suppose that the response variable R_z, can be predicted by quadratic model as follows,

$$R_x = 2.1-0.225 \cdot v + 198.25 \cdot f + 1.175 \cdot d$$
 (8)

Where; R_z is the surface roughness in μm , v is the cutting speed (m min⁻¹), f is the federate (mm rev⁻¹), d is the depth of cut (mm), $c_0,...,c_q$ are constants.

Table 3 shows the resulting ANOVA table for reduced quadratic model. The results second-order model will be:

$$R_z = 24.80-2.48 \cdot v + 9.91 \cdot f + 0.59 \cdot d$$

$$-1.05 \cdot v \cdot f - 0.52 \cdot v \cdot d + 0.36 \cdot f \cdot d$$

$$+0.38 \cdot v^2 + 0.69 \cdot f^2 + 0.063 \cdot d^2$$
(9)

Table 3: The resulting ANOVA table for reduced quadratic model

	Sum of		Mean	F	p-value
Source	squares	df	square	value	prob>F
Model	1094.24	9	118.26	17.35	< 0.001
A-cutting spread	61.26	1	61.26	8.99	0.0134
B-feed rate	982.58	1	982.58	144.16	< 0.0001
C-depth of cut	3.45	1	3.45	0.51	0.4930
AB	8.77	1	8.77	1.29	0.2832
AC	2.13	1	2.13	0.31	0.5887
BC	1.03	1	1.03	0.15	0.7052
A^2	0.39	1	0.39	0.57	0.8165
B^2	1.30	1	1.30	0.19	0.6716
C^2	0.011	1	0.011	1.576	0.9691
Residual	68.16	10	6.82		
Lack of fit	2.61	4	0.52	0.040	0.9985 ^{NS}
Pure error	65.55	5	13.11		
Cor total	1132.40	19			

NS: Not Significant

Table 4: Mod	lel summary static		
Std. Dev.	2.35	R. squared	0.9367
Mean	24.77	Adj R-squared	0.9074
CV %	9.48	Pred R-squared	0.9062
Press	106.04	Adeq precision	19.968

As in Table 4, R-Squared value is high, close to 1, which is desirable. The predicted is in reasonable agreement with the adjusted R-Squared.

The adjusted R-Squared value is particularly useful when comparing models with different number of terms (Choudhury and El-Baradie, 1999). This comparison is however done in the background when model reduction is taking place. Adequate precision compares the range of the predicted values at design points to the average prediction error. Ratios greater than 4 indicate adequate model discrimination. In this particular case the value is well above 4.

EXPONENTIAL MODEL

The proposed relationship between the surface roughness and machining independent variables can be represented by the following:

$$R_{\tau} = c.v^{\alpha}.f^{\beta}.d^{\gamma}.\varepsilon \tag{10}$$

Where; R_z is the surface roughness in μm , v is the cutting speed (m min⁻¹), f is the federate (mm rev⁻¹), d is the depth of cut (mm), ϵ is random error and c, α , β , γ are constants.

A linear model can be obtained for surface roughness by applying a logarithmic transformation to Eq. 10.

$$\ln R_z = \ln c + \alpha \ln v + \beta \ln f + \gamma \ln d + \ln \varepsilon \tag{11}$$

Equation 11 may be represented by the following general statistical form:

$$\hat{y} = y - \varepsilon = b_0 x_0 + b_1 x_1 + b_2 x_2 + b_3 x_3$$
 (12)

 $\boldsymbol{\epsilon}$ is random error and b values are the estimates of model parameters.

Where \hat{y} is the estimated response of surface roughness on logarithmic scale, y is the measured response on logarithmic scale, $x_0 = 1$, $x_1 = \ln v$, $x_2 = \ln f$, $x_3 = \ln d$ Thus

$$\ln R_z = +6.44902 - 0.28144 \cdot \ln v$$

+1.16497 \cdot \ln f + 0.036215 \cdot \ln d

$$R_z = 632.082 \text{ v}^{-0.28144} \text{ f}^{+1.16497} \text{ d}^{+0.036215}$$
 (14)

Figure 1 shows the estimated R_z as a function of Cutting speed and Feed rate, the height of the surface represents the value of R_z .

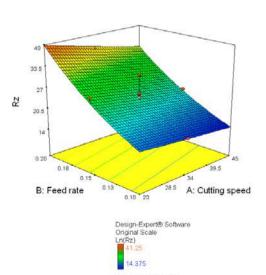


Fig. 1: R_z(μm) as a function of cutting speed (m min⁻¹) and feed rate (mm rev⁻¹)

Actual Factor C: Depth of cut = 1.00

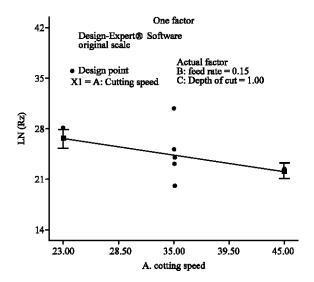


Fig. 2: Graf shows the single effect of cutting speed (m min⁻¹)

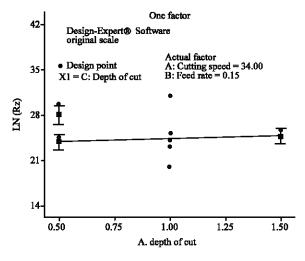


Fig. 3: Graf shows the single effect of depth of cut (mm)

Figure 2 and 3 show the single effect of cutting speed and depth of cut, respectively.

RESULTS AND DISCUSSION

This research presented a factorial experimentation approach to studding the impact of turning parameters on surface roughness. The results show that depth of cut does not impact the surface roughness in the studied range, which could be used to improve productivity if it would not worsen the surface microstructure of the material and the dimensional and geometric accuracy.

The results for analysis of variance for the secondorder model reveal that the interaction terms and the square terms are statistically insignificant. The established equation clearly shows that the feed rate is the most influencing factor on surface roughness. However, it follows by cutting speed. Surface roughness increased by increasing feed rate while decrease with increasing cutting speed.

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